

Application of Model Assisted Probability of Detection (MAPOD) to a Guided Wave SHM System

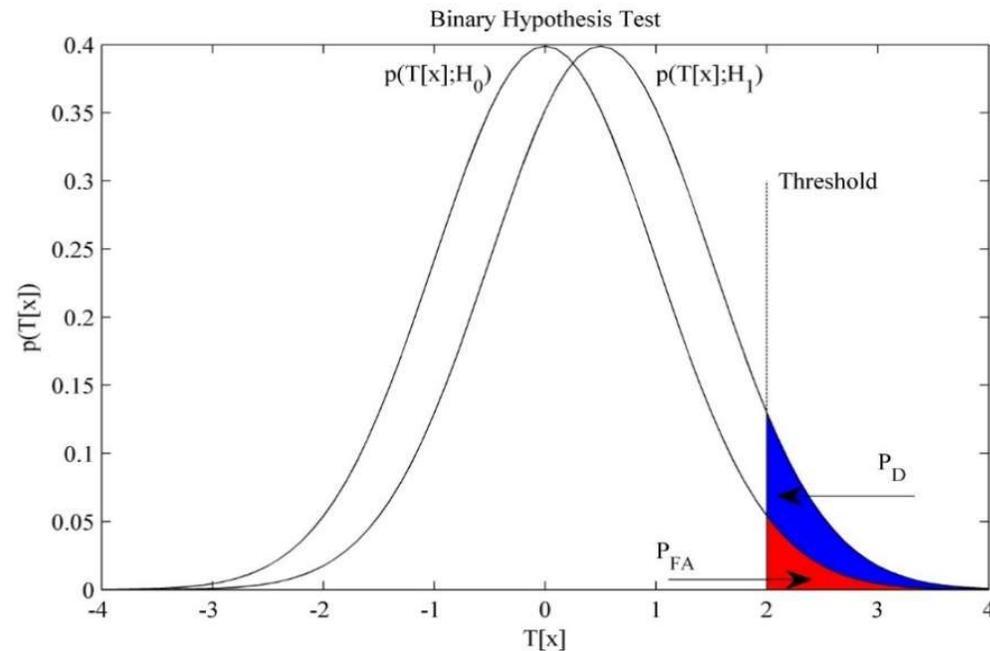
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*structural health monitoring
multi-functional materials
lean enterprise solutions*

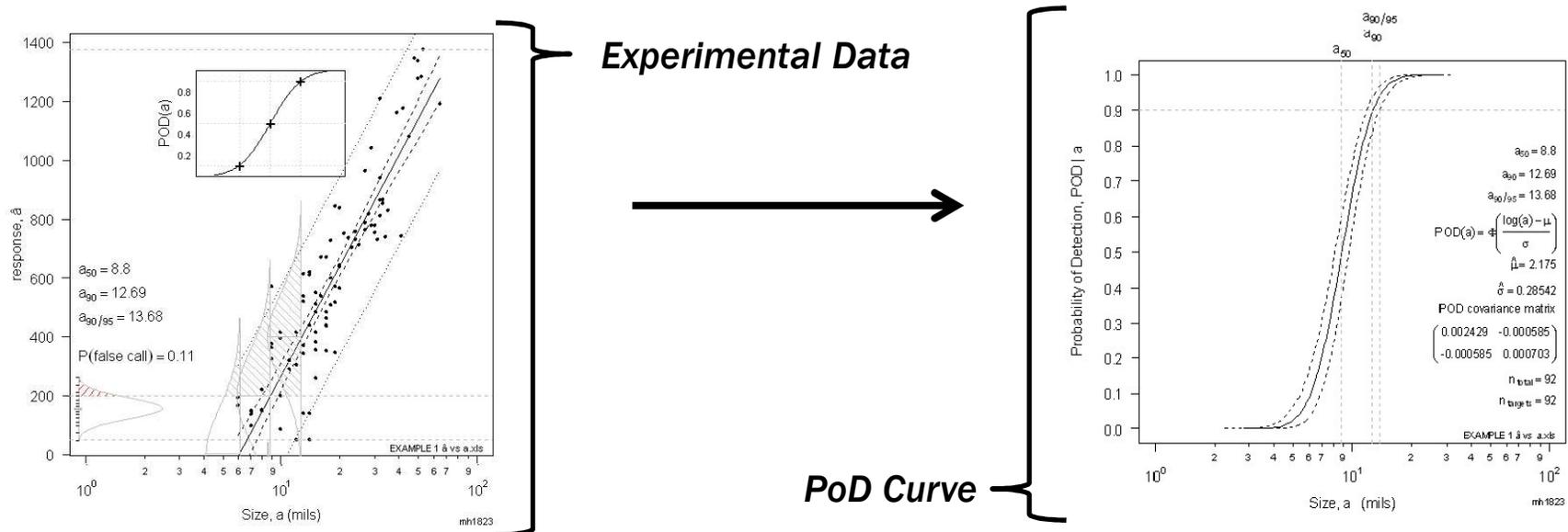
What is Probability of Detection?

- **Binary hypothesis test**
 - **X** is data
 - **T[x]** is signal processing algorithm (“detector”)
 - **P(T[x])** is probability density function for a given state **H**



Damage Tolerant Design & Probability of Detection

- Damage tolerant approach common for DoD/commercial design
 - Requires definition of minimum detectable flaw size
 - Requires inspection interval set to find minimum flaw with safety factor
- $a_{90/95}$ is flaw size found 90% of the time with 95% confidence
 - MIL-HDBK 1823A establishes guidelines for NDE reliability assessment
 - Probability of Detection (PoD) method presented to determine $a_{90/95}$

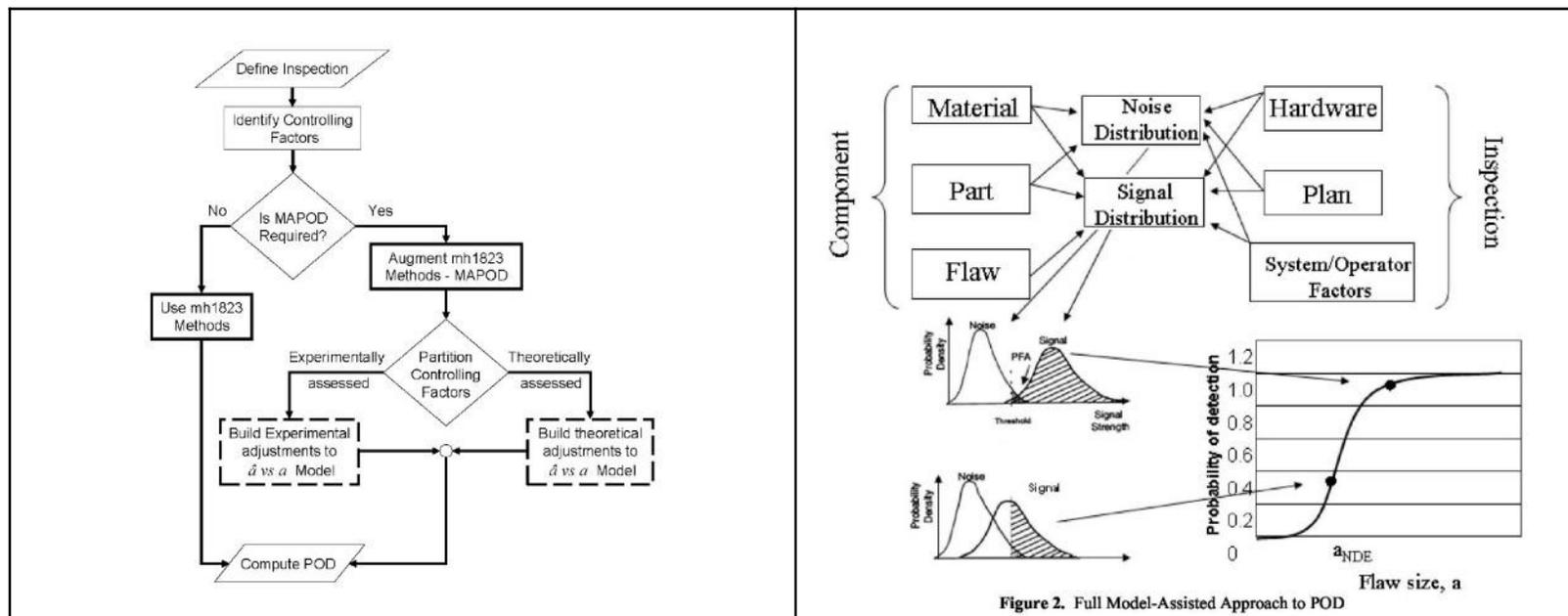


PoD for Structural Health Monitoring

- **SHM methods differ from NDE methods**
 - SHM sensors are generally integrated into a structure permanently
 - SHM monitors an area, not a point: PoD a function of distance/orientation
 - Sources of variability: bonding, temperature, loading conditions, ect.
- **Difficult to establish POD for SHM for all variations of parameters**
- **Model Assisted POD (MAPOD) becomes essential**
- ***Must use model assisted POD (MAPOD) for SHM systems***
 - *Sources of variability are integrated into experimentally updated models*

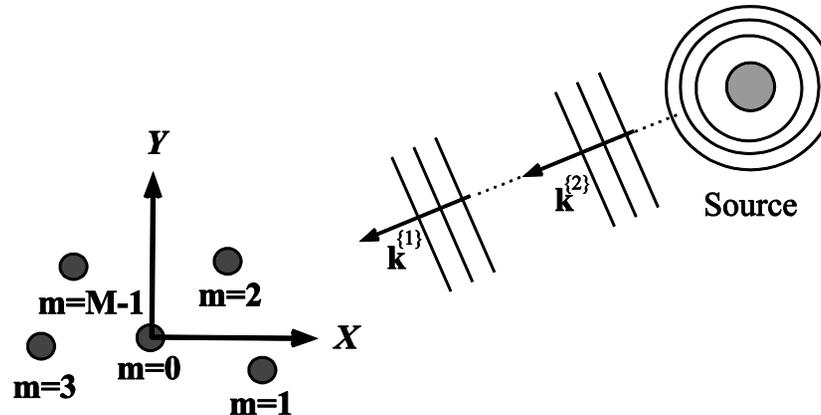
MAPOD

- MAPOD allows use of theoretical models to compute POD
 - Traditional 1823a only experimental based
 - Theoretical models can include:
 - wave attenuation in bulk material due to change in inspection distance
 - change of material type (AL 6061 to AL 7075) etc.



Active Sensing Guided Wave Model (1)

- Assume signal model



$$\tilde{s}_m [n] = A^{A_0} \exp[\phi^{A_0}] \Pi^{A_0} [n, r] \exp[j2\pi fn] \exp[-j2\pi f \tau_m^{A_0}]$$

- The signal at the sensor m is narrow band
 - Phase shift due to inter-element spacing as multiplying factor

Active Sensing Guided Wave Model (2)

- Under state of noise only

$$p(\tilde{\mathbf{x}}; H_0)$$

- Under state of signal plus noise

$$p(\tilde{\mathbf{x}}; \boldsymbol{\theta}_1, H_1)$$

- Generalized Likelihood ratio test: maximize POD for fixed false alarm rate

$$L_G(\tilde{\mathbf{x}}) = \frac{p(\tilde{\mathbf{x}}; \boldsymbol{\theta}_1, H_1)}{p(\tilde{\mathbf{x}}; H_0)} > \gamma'$$

- Resulting detector is

$$T(\tilde{\mathbf{x}}) = \frac{2}{\sigma^2 ((KM)^2)} \left[|\mathbf{h}_1^H \tilde{\mathbf{x}}|^2 + |\mathbf{h}_2^H \tilde{\mathbf{x}}|^2 \right]$$

where

$$|\mathbf{h}_1^H \tilde{\mathbf{x}}|^2 = \left| \sum_{m=0}^{M-1} \sum_{n=0}^{N-1} \tilde{x}_m[n] \Pi^{A_0}[n, r] \exp[-j2\pi f(n - \tau_m^{A_0})] \right|^2$$

Active Sensing Guided Wave Model (3)

- **Resulting closed form statistics of detector are Chi-squared distributed**

➤ **Probability of false alarm detection** $P_{FA} = Q_{\chi^2_2}(\gamma')$

➤ **Probability of detection** $P_D = Q_{\chi^2_2(\lambda_1)}(\gamma')$

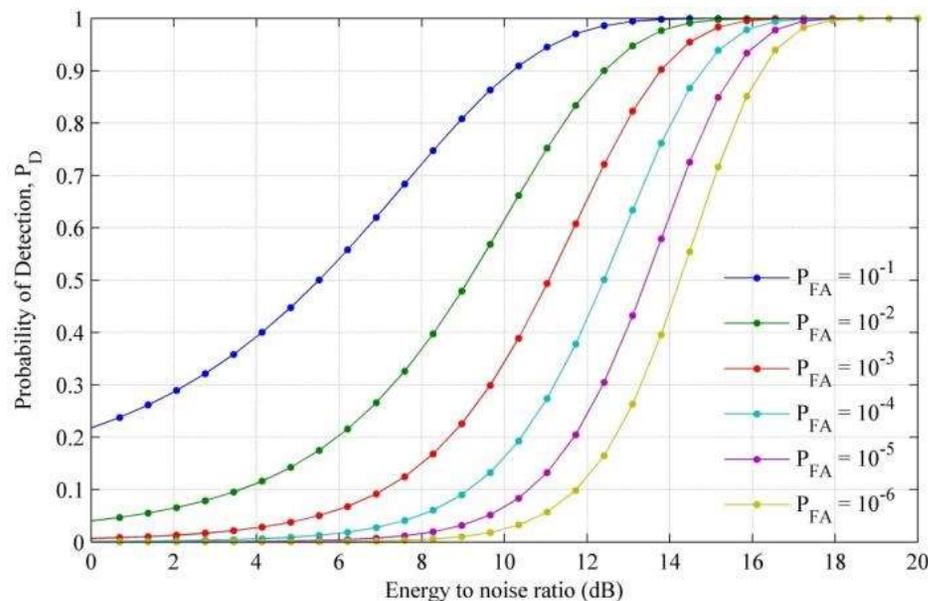
➤ **Import parameter is the non-centrality parameter**

$$\lambda_1 = \frac{A^2 MN}{\sigma^2 / 2}$$

➤ **This is the energy to noise ratio (ENR)**

Active Sensing Guided Wave Model (4)

- POD curve is results of varying the SNR ratio

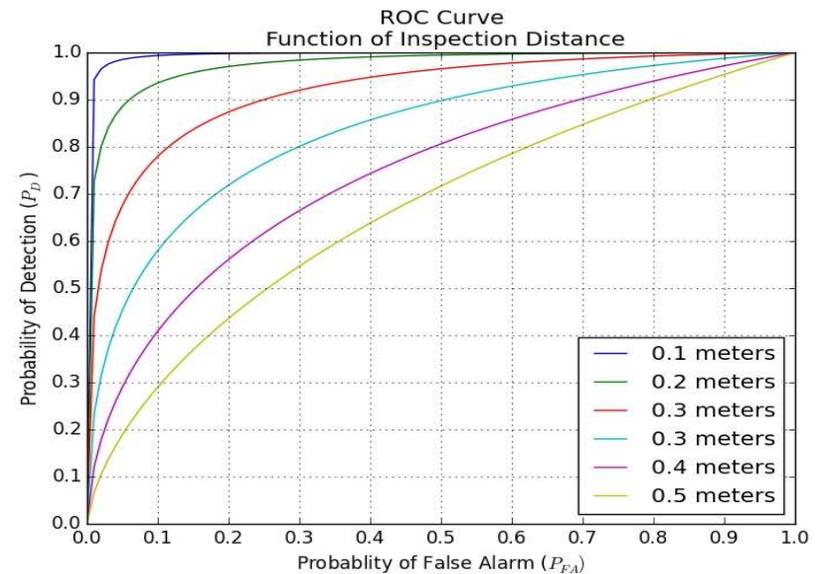
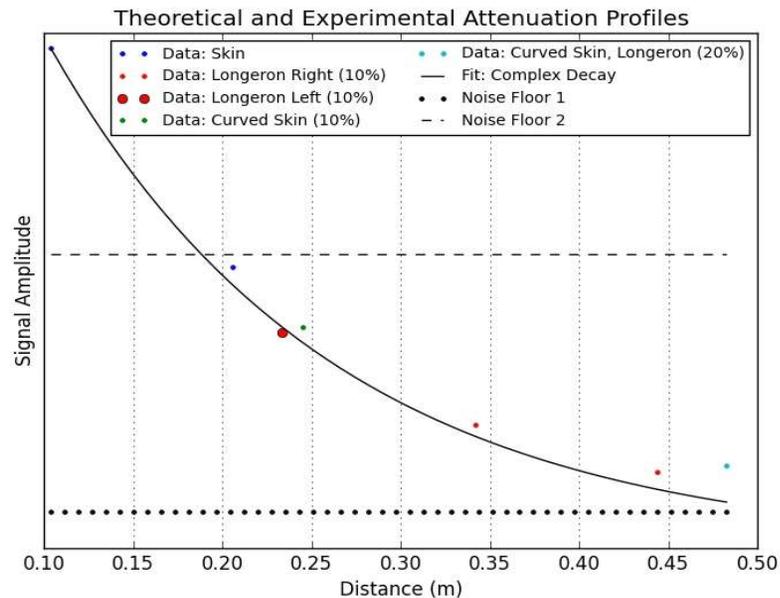


$$\lambda_1 = \frac{A^2 MN}{\sigma^2 / 2}$$

- Assuming “far” scattering field
 - Parameterize A as $A(x)$
 - Scattering amplitude is now a function of the material attenuation profile
 - Allows for calculation of POD as a function of distance to damage

Attenuation Model

- Incorporate theoretical attenuation to transform POD as a function of distance
 - Model updating of attenuation profile with experimental data



Application parameters

- **Under what conditions can this be applied**
 - Only when underlying sources of variability remain unchanged
 - Change in like material type
 - Aluminum to steel,
 - Decrease in uncorrelated noise environment
 - Upgraded A/D

- **Under what conditions can this NOT be applied**
 - Aluminum to carbon fiber
 - Changes in material thickness
 - Unless scattering of new wave number is shown to scale accordingly
 - Also there cannot be a change to PZT actuator/sensor resonant characteristics
 - Signal model is not valid
 - Correlated noise
 - Orthogonality of guided wave modes

Summary

- **Differentiation between SHM & NDI for reliability assessment**
 - SHM permanently installed at a point to cover an area, cost driver
 - Different variables effect PoD (temperature), no operator
- **MAPOD becomes essential in order to implement POD for SHM**
 - Reduce physical test matrix size with models to minimize cost
- **Basic guided wave signal model results in detector with closed form statistics**
 - POD is driven by ENR or SNR which correlates to signal amplitude
- **Implementation of MAPOD techniques is application specific**

Future Work

- **Building analytical tools under NAVAIR SBIR funding in order to facilitate MAPOD for guided wave SHM in metallic structures**
- **Conducting validation experiments for guided wave SHM**
 - **Metallic structures for crack growth**
 - **Composite structures for delamination**
- **Main focus initially on demonstration of validity of distance to damage MAPOD approach for metallic applications**
 - **Next will look at influence of geometry**
 - **Then will investigate limits of applicability with thickness changes**

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